

JC542 U.S. PTO
09/294563
04/20/99

**APPENDIX 2
FOR APPLICATION**

FOR

UNITED STATES LETTERS PATENT

**TITLE: PREDICTING PERFORMANCE OF TELEPHONE LINES FOR
DATA SERVICES**

APPLICANT: KURT E. SCHMIDT, DAVID J. GROESSL AND YUN ZHANG

"EXPRESS MAIL" Mailing Label Number EL245467840US

Date of Deposit April 20, 1999

I hereby certify under 37 CFR 1.10 that this correspondence is being deposited with the United States Postal Service as "Express Mail Post Office To Addressee" with sufficient postage on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, D.C. 20231.

Kristy Cioffi
Kristy Cioffi

Appendix 2

30Hz Raw Measurements:

Ytr(30) - Admittance tip-to-ring measured at 30Hz
 Ytg(30) - Admittance tip-to-ground measured at 30Hz
 Yrg(30) - Admittance ring-to-ground measured at 30Hz

30Hz Derived Measurements:

30Gtr - Conductance tip-to-ring measured at 30Hz = $\text{real}(\text{Ytr}(30))$
 30Str - Susceptance tip-to-ring measured at 30Hz = $\text{imag}(\text{Ytr}(30))$
 30Gtg - Conductance tip-to-ground measured at 30Hz = $\text{real}(\text{Ytg}(30))$
 30Stg - Susceptance tip-to-ground measured at 30Hz = $\text{imag}(\text{Ytg}(30))$
 30Ctr - Capacitance tip-to-ring measured at 30Hz = $\text{Str}(30)/(2 \cdot \pi \cdot 30)$
 30Ctg - Capacitance tip-to-ground measured at 30Hz = $\text{Stg}(30)/(2 \cdot \pi \cdot 30)$
 Lmeas - Length in kft measured at 30Hz = $30\text{Ctg}/17.47$

150Hz-20KHz Raw Measurements:

Ytr(f) - Admittance tip-to-ring where $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$
 Ytg(f) - Admittance tip-to-ground where $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$
 Yrg(f) - Admittance ring-to-ground where $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$

150Hz-20KHz Derived Measurements:

150Gtr - Conductance tip-to-ring measured at 150Hz = $\text{real}(\text{Ytr}(150))$
 600Gtr - Conductance tip-to-ring measured at 600Hz = $\text{real}(\text{Ytr}(600))$

 19950Gtr - Conductance tip-to-ring measured at 19950Hz = $\text{real}(\text{Ytr}(19950))$

 150Str - Susceptance tip-to-ring measured at 150Hz = $\text{imag}(\text{Ytr}(150))$
 600Str - Susceptance tip-to-ring measured at 600Hz = $\text{imag}(\text{Ytr}(600))$

 19950Str - Susceptance tip-to-ring measured at 19950Hz = $\text{imag}(\text{Ytr}(19950))$

 150Gtg - Conductance tip-to-ground measured at 150Hz = $\text{real}(\text{Ytg}(150))$
 600Gtg - Conductance tip-to-ground measured at 600Hz = $\text{real}(\text{Ytg}(600))$

 19950Gtg - Conductance tip-to-ground measured at 19950Hz = $\text{real}(\text{Ytg}(19950))$

 150Stg - Susceptance tip-to-ground measured at 150Hz = $\text{imag}(\text{Ytg}(150))$
 600Stg - Susceptance tip-to-ground measured at 600Hz = $\text{imag}(\text{Ytg}(600))$

 19950Stg - Susceptance tip-to-ground measured at 19950Hz = $\text{imag}(\text{Ytg}(19950))$

 150Ctr - Capacitance tip-to-ring measured at 150Hz = $150\text{Str}/(2 \cdot \pi \cdot 150)$
 600Ctr - Capacitance tip-to-ring measured at 600Hz = $600\text{Str}/(2 \cdot \pi \cdot 600)$

 19950Ctr - Capacitance tip-to-ring measured at 19950Hz = $19950\text{Str}/(2 \cdot \pi \cdot 19950)$

 150Ctg - Capacitance tip-to-ground measured at 150Hz = $150\text{Stg}/(2 \cdot \pi \cdot 150)$
 600Ctg - Capacitance tip-to-ground measured at 600Hz = $600\text{Stg}/(2 \cdot \pi \cdot 600)$

 19950Ctg - Capacitance tip-to-ground measured at 19950Hz = $19950\text{Stg}/(2 \cdot \pi \cdot 19950)$

150Hz-20KHz Secondary Derived Measurements:

C30/C4K - Ratio of tip-to-ground Capacitance at 30Hz to 4200Hz
 C4K/C10K - Ratio of tip-to-ground Capacitance at 4200Hz to 10050Hz
 Cslope - Tip-to-ground Capacitance ratio slope = $(C4K/C10K)/(C30/C4K)$
 C30-C4K - Difference in tip-to-ground Capacitance at 30Hz and 4200Hz
 C4K-C10K - Difference in tip-to-ground Capacitance at 4200Hz and 10050Hz
 Cdelta - Tip-to-ground Capacitance difference delta = $(C4K-C10K)/(C30-C4K)$

G4K/G30 - Ratio of tip-to-ground Conductance at 4200Hz to 30Hz
 G10K/G4K - Ratio of tip-to-ground Conductance at 10050Hz to 4200Hz
 Gslope - Tip-to-ground Conductance ratio slope = $(G10K/G4K)/(G4K/G30)$
 G4K-G30 - Difference in tip-to-ground Conductance at 30Hz and 4200Hz
 G10K-G4K - Difference in tip-to-ground Conductance at 4200Hz and 10050Hz
 Gdelta - Tip-to-ground Conductance difference delta = $(G10K-G4K)/(G4K-G30)$

C30/G30 - Ratio of Tip-to-ground Capacitance to Conductance at 30Hz
 C30/G4K - Ratio of Tip-to-ground Capacitance at 30Hz to Conductance at 4200Hz
 C4K/G4K - Ratio of Tip-to-ground Capacitance to Conductance at 4200Hz

Gtr_dmax - Maximum positive slope of $Gtr(f) = \max(\text{derivative}(Gtr(f)/df))$
 Gtr_fmax - Frequency at which Gtr_dmax occurs
 Gtr_dmin - Maximum negative slope of $Gtr(f) = \min(\text{derivative}(Gtr(f)/df))$
 Gtr_fmin - Frequency at which Gtr_dmin occurs
 Gtr_fpk - Frequency of first peak (local maxima) in $Gtr(f)$
 Gtr_fval - Frequency of first valley (local minima) in $Gtr(f)$
 Gtr_d_delta - Gtr Max/Min Derivative difference = $Gtr_dmax - Gtr_dmin$
 Gtr_pk_delta - Gtr peak/valley frequency difference = $Gtr_fval - Gtr_fpk$
 Gtr_pk - Value of $Gtr(f)$ at frequency Gtr_fval
 Gtr_val - Value of $Gtr(f)$ at frequency Gtr_fval
 Gtr_delta - Gtr peak/valley difference = $Gtr_pk - Gtr_val$

Gtg_dmax - Maximum positive slope of $Gtg(f) = \max(\text{derivative}(Gtg(f)/df))$
 Gtg_fmax - Frequency at which Gtg_dmax occurs
 Gtg_dmin - Maximum negative slope of $Gtg(f) = \min(\text{derivative}(Gtg(f)/df))$
 Gtg_fmin - Frequency at which Gtg_dmin occurs
 Gtg_d_delta - Gtg Max/Min Derivative difference = $Gtg_dmax - Gtg_dmin$

Ctr_dmax - Maximum positive slope of $Ctr(f) = \max(\text{derivative}(Ctr(f)/df))$
 Ctr_fmax - Frequency at which Ctr_dmax occurs
 Ctr_dmin - Maximum negative slope of $Ctr(f) = \min(\text{derivative}(Ctr(f)/df))$
 Ctr_fmin - Frequency at which Ctr_dmin occurs
 Ctr_fpk - Frequency of first peak (local maxima) in $Ctr(f)$
 Ctr_fval - Frequency of first valley (local minima) in $Ctr(f)$
 Ctr_d_delta - Ctr Max/Min Derivative difference = $Ctr_dmax - Ctr_dmin$
 Ctr_pk_delta - Ctr peak/valley frequency difference = $Ctr_fval - Ctr_fpk$
 Ctr_val - Value of $Ctr(f)$ at frequency Ctr_fval

Ctg_dmax - Maximum positive slope of $Ctg(f) = \max(\text{derivative}(Ctg(f)/df))$
 Ctg_fmax - Frequency at which Ctg_dmax occurs
 Ctg_dmin - Maximum negative slope of $Ctg(f) = \min(\text{derivative}(Ctg(f)/df))$
 Ctg_fmin - Frequency at which Ctg_dmin occurs
 Ctg_d_delta - Ctg Max/Min Derivative difference = $Ctg_dmax - Ctg_dmin$

Str_dmax - Maximum positive slope of $Str(f) = \max(\text{derivative}(Str(f)/df))$
 Str_fmax - Frequency at which Str_dmax occurs
 Str_dmin - Maximum negative slope of $Str(f) = \min(\text{derivative}(Str(f)/df))$
 Str_fmin - Frequency at which Str_dmin occurs

150Hz-20KHz Secondary Derived Measurements:

Str_fpk - Frequency of first peak (local maxima) in Str(f)
Str_fval - Frequency of first valley (local minima) in Str(f)
Str_d_delta - Str Max/Min Derivative difference = Str_dmax-Str_dmin
Str_pk_delta - Str peak/valley frequency difference = Str_fval-Str_fpk
Str_pk - Value of Str(f) at frequency Str_fpk
Str_val - Value of Str(f) at frequency Str_fval
Str_delta - Str peak/valley difference = Str_pk-Str_val

Stg_dmax - Maximum positive slope of Stg(f) = max(derivative(Stg(f)/df))
Stg_fmax - Frequency at which Stg_dmax occurs
Stg_dmin - Maximum negative slope of Stg(f) = min(derivative(Stg(f)/df))
Stg_fmin - Frequency at which Stg_dmin occurs
Stg_fpk - Frequency of first peak (local maxima) in Stg(f)
Stg_fval - Frequency of first valley (local minima) in Stg(f)
Stg_d_delta - Stg Max/Min Derivative difference = Stg_dmax-Stg_dmin
Stg_pk_delta - Stg peak/valley frequency difference = Stg_fval-Stg_fpk

Gtg20k/Gtg8k - Ratio of Gtg at 19950Hz and 8250Hz
Gtg20k/Gtg4k - Ratio of Gtg at 19950Hz and 4200Hz
Cgt30/Cgt20k - Ratio of Ctg at 30Hz and 19950Hz
Cgt30/Cgt8k - Ratio of Ctg at 30Hz and 8250Hz